

## Errata

T. Y. Otoshi, S. R. Stewart, and M. M. Franco have submitted the following errata to "A Portable X-Band Front-End Test Package for Beam-Waveguide Antenna Performance Evaluation—Part I: Design and Ground Tests" that appeared in *The Telecommunications and Data Acquisition Progress Report 42-103*, vol. July–September 1990, pp. 135–150. The last sentence of the third paragraph on page 137 should be replaced with:

The corrected system temperature is obtained by multiplying each point by the corresponding linearity factor shown in Fig. 10(a) [5]. However, it can be seen that the corrected value would be different by about only 1 percent. It should be pointed out that in this article the above term "uncorrected" measured operating system noise temperature was used to refer to the system temperature that had already corrected for gain change, but not corrected for nonlinearity.

## Errata

N. R. Mysoor, J. D. Perret, and A. W. Kermode have submitted the following errata to "Design Concepts and Performance of NASA X-Band (7162 MHz/8415 MHz) Transponder for Deep-Space Spacecraft Applications" that appeared in *The Telecommunications and Data Acquisition Progress Report 42-104*, vol. October-December 1990, pp. 247-256. Table 2 and Figure 1 should be replaced with the table and figure on the following pages.

Table 2. Transponder carrier phase tracking loop parameters

Transponder	Design		Threshold, $\alpha_0 = 0.0531$				Signal condition				Strong signal, 50 dB above threshold, $\alpha_S = 1.0$		
	$K_v$ , $\text{sec}^{-1}$	$\tau_1$ , sec	$\tau_2$ , sec	$\zeta_0$	$\omega_{n_0}$ , rad/sec	$2B_{L_0}$ , Hz	$\zeta_{10}$	$\omega_{n_{10}}$ , rad/sec	$2B_{L_{10}}$ , Hz	$\zeta_S$	$\omega_{n_S}$ , rad/sec	$2B_{L_S}$ , Hz	$\Delta\omega$ , Hz/sec
NST	$1.44 \times 10^7$	2910	0.0833	0.68	16.2	17.0	1.20	40.3	28.7	2.90	70.3	209.9	394
NST + XSDC	$4.88 \times 10^7$	2910	0.0833	1.24	29.8	43.1	2.20	52.8	122.3	5.39	129.5	704.5	1334
GLL	$1.62 \times 10^7$	3732	0.0423	0.32	15.2	16.7	0.57	27.1	26.9	1.42	66.0	105.3	347
GLL + XSDC	$5.73 \times 10^7$	3732	0.0423	0.73	34.1	36.6	1.30	90.0	60.4	2.66	123.9	341.2	1222
MAG	$1.44 \times 10^7$	728	0.0208	0.42	40.4	41.0	1.49	118.3	71.5	1.50	126.0	210.0	1263
MAG + XSDC	$4.88 \times 10^7$	728	0.0208	0.62	59.7	61.6	1.10	105.6	140.1	2.69	258.9	721.2	5335
DST	$2.2 \times 10^7$	3556	0.0556	0.50	18.0	18.0	0.88	31.9	37.2	2.17	78.1	178.5	550

$K_v$  = DC gain of the PLL,  $\text{sec}^{-1}$

$\tau_1$  = Time constant associated with the open-loop pole (phase lag) of the loop filter, sec

$\tau_2$  = Time constant associated with the open-loop zero (phase lead) of the loop filter, sec

$\alpha_0$ ,  $\alpha_{10}$ ,  $\alpha_S$  = Limiter suppression factor at threshold, 10 dB above threshold, and strong signal

$\zeta_0$ ,  $\zeta_{10}$ ,  $\zeta_S$  = PLL damping factor at threshold, 10 dB above threshold, and strong signal

$\omega_{n_0}$ ,  $\omega_{n_{10}}$ ,  $\omega_{n_S}$  = PLL natural frequency at threshold, 10 dB above threshold, and strong signal, rad/sec

$2B_{L_0}$ ,  $2B_{L_{10}}$ ,  $2B_{L_S}$  = PLL noise-equivalent bandwidth at threshold, 10 dB above threshold, and strong signal, Hz

$\Delta\omega$  = PLL acquisition and tracking rate at strong signal, Hz/sec

NST = NASA Standard DST (S-band)

GLL = Galileo transponder (S-band)

MAG = Magellan transponder (S-band)

DST = Deep space transponder (X-band design)

XSDC = External X-band to S-band downconverter

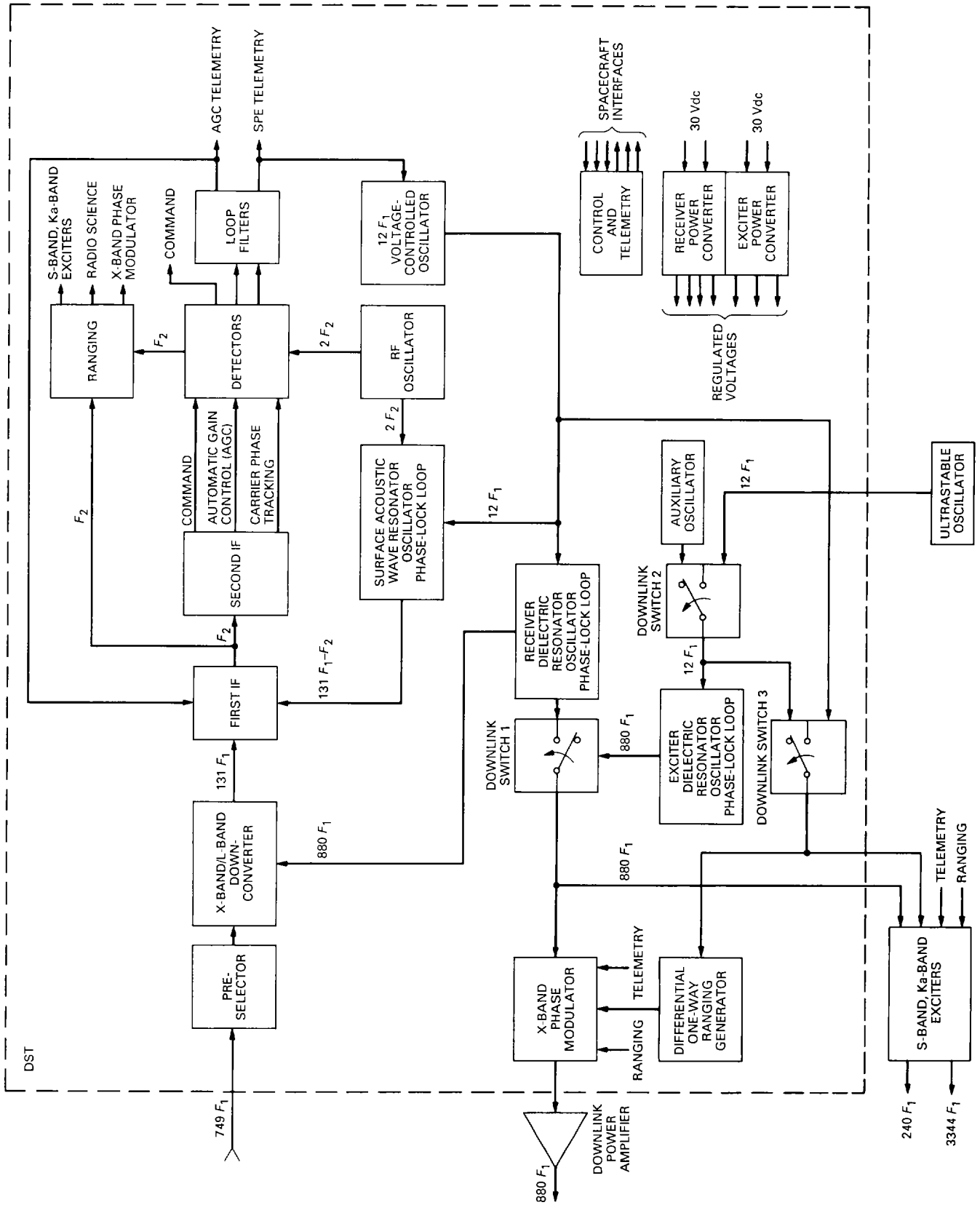


Fig. 1. Deep-space transponder.